

On Page 31, Paragraph 4:

The spot diameter ϕ_1 on focussing is given by

$$\begin{aligned} & (S_{pp}/2) \times 2 \times (\beta_A \times \beta_2)^2 \times \{(2 \cdot NA)/(\beta_A \times \beta_2)\} \\ & = 2 \cdot NA \cdot S_{pp} \cdot (\beta_A \times \beta_2) \end{aligned}$$

...(1).

On Page 32, Paragraph 1:

If, in the above equation 1, the focussing pull-in range S_p is fixed and the spot diameter ϕ_1 on focussing is fixed, the spot diameter ϕ_1 is given by

$$\phi = 2 \cdot NA \cdot S_{pp} \cdot (\beta_A \times \beta_2) = \text{constant}$$

so that the multiplication factor β_2 for the direction 2 for detecting the tracking error and the land-groove discrimination signal is in proportion to $1/\beta_A$.

$$\beta_2 \propto 1/\beta_A$$

So, the variation of the spot diameter ϕ_2 for the defocussing Δ_{def} is

$$\Delta\phi_2/\Delta_{Def} \propto 4 \cdot NA \cdot \beta_2 \propto 1/\beta_A$$

...(3)

so that it is inversely proportional to the multiplication factor β_A of the anamorphic prism. Meanwhile, if the direction of the multiplication factor of the anamorphic prism is the radial direction, it suffices to substitute $1/\beta_A$ for β_A .

REMARKS

This preliminary amendment is filed to correct the specification. If the Examiner has any suggestions for placing this application in even better form, the Examiner is invited to telephone